

LASER INTERFEROMETER GRAVITATIONAL WAVE OBSERVATORY  
- LIGO -  
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**Multiply Resonant EOM for the  
LIGO 40-meter Interferometer**

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**Abstract**

The Laser Interferometer Gravitational-Wave Observatory (LIGO) uses a Michelson interferometer with Fabry-Perot cavities to sense strains induced by gravitational waves. Length sensing and control is achieved through locking the optical cavity lengths to the laser wavelength. For locking, an electro-optic modulator (EOM) is utilized to modulate the phase, creating frequency sidebands. For the upgrade of the 40-meter prototype interferometer, used to test systems before implementation in the full-scale observatories, there will be three modulation frequencies: 11 and 55, and 29.5 MHz, used for control of the mirrors in the main interferometer and mode cleaner, respectively. The purpose of this project was to design, build and test a triply resonant circuit for the 40-m upgrade, allowing three modulations to occur inside one EOM rather than several, reducing wavefront deformation, power loss, and problems with alignment. Resonance will allow for lower driving voltages and suppression of harmonics. The designed circuit has resonance at the necessary frequencies, with roughly equivalent gain and an impedance of  $50 \Omega$  at each peak. Several iterations of the circuit were built, and the performance of each was evaluated by measuring the transfer function and impedance, and by observing the sidebands using an optical spectrum analyzer.

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# 1 Background and Motivation

The Laser Interferometer Gravitational-Wave Observatory (LIGO) uses a Michelson interferometer with Fabry-Perot cavities to detect strains induced by gravitational waves. Fabry-Perot cavities use resonance to increase sensitivity to length displacements; to remain at resonance, the cavity length must be an integer multiple of the wavelength of laser light used. To maintain the length for resonance, a feedback system is used; because the intensity will be the same on either side of resonance, modulation of the laser is used to distinguish between situations where the cavity length is too short and too long. This modulation is provided by an electro-optic modulator (EOM) [1, 2].

An EOM is an optical device that modulates the phase, polarization, or amplitude of light according to an electrical voltage signal. The indices of refraction of certain crystals are sensitive to electric fields; this property of a crystal can be exploited to create phase and polarization variations in light passed through the crystal (amplitude modulations are achieved by varying the polarization and passing the light through a polarizer). EOMs can be either resonant or broadband; a resonant EOM contains an LC circuit to create electrical resonance, which means that the input voltage can be much lower than the voltage across the crystal, while a broadband EOM does not contain this component and can be used to generate modulations of a wide range of frequencies. Resonant EOMs can only produce modulations at specific frequencies [3].

In LIGO, the EOM modulates the phase of the laser. Effectively, this phase modulation creates two frequency sidebands in the laser beam: one at the sum of the frequency of the laser light and the frequency of modulation, and one at the difference between them. As the modulated light enters a resonant cavity, a certain fraction of the light is reflected; this quantity depends on both the frequency of the incident beam and the length of the optical cavity. Because of this, it is possible to detect fluctuations in the cavity length as fluctuations in the power of the reflected light. Furthermore, through analysis of the relative power of the frequency components of the reflected beam, the direction of length displacement (too short or too long for resonance) can also be determined. To do this, the reflected power signal is mixed with the modulation signal to produce an error signal which is proportional to the displacement from resonance when the cavity length is close to resonance. This signal is used to drive a servo to control the length of the cavity, creating a feedback loop that keeps the cavity at resonance; since the signal represents the cavity length's deviation from resonance, it is also the signal with which gravitational waves will be detected. [1].

Currently, modulation is produced by two EOMs in a Mach-Zehnder interferometer configuration. The two main modulation frequencies are 33 and 166 MHz, and the mode cleaner modulation frequency is 29 MHz; since 29 MHz is close to 33 MHz, this modulation can be produced by driving the 33 MHz resonant EOM at the desired frequency. The Mach-Zehnder configuration increases the complexity of the setup, and its alignment affects the alignment going into the main interferometer. For the 40-m upgrade, the three modulations will occur in a single EOM, reducing the complexity that the Mach-Zehnder introduces [5]. Using fewer EOMs will also reduce wavefront distortion and power loss. While it would be possible to drive a broadband EOM at the three modulation frequencies, a resonant circuit will make it possible to drive the circuit with a low-amplitude voltage, while still maintaining a high voltage across the EOM. It also suppression of the harmonics of the driving frequencies.

For the 40-m upgrade, two sets of sidebands will be used for length and alignment sensing, and one set will be necessary to control the mode cleaner; therefore, three sets of sidebands must be created. This will be achieved by creating an EOM circuit with triple resonance. The goal of this project will be to design, analyze, and test a triply resonant EOM for the upgrade of the 40-m prototype interferometer. This EOM will then be used to induce the three modulation frequencies necessary for locking and length sensing (GW detection). If successful, by the end of the project, a working prototype of the triply resonant EOM should exist [4].

## 2 Circuit Design

### 2.1 Conceptual Design

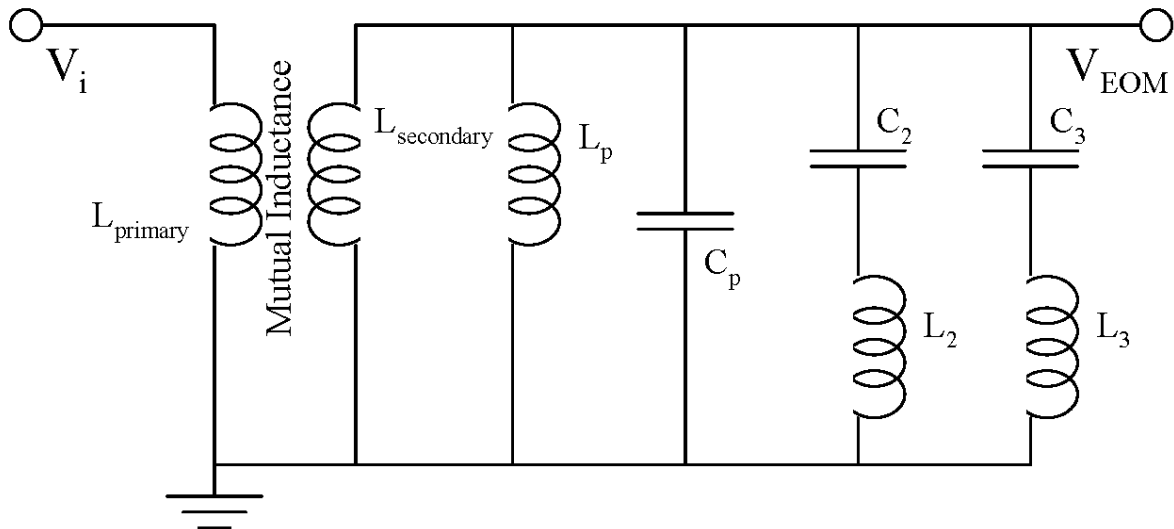


Figure 1: EOM circuit diagram

The basic conceptual design of the circuit is shown in Figure 1. Generally, this circuit creates the three necessary resonant peaks by creating one resonant peak, and two valleys within it. The inductance in the transformer and the inductor parallel to it, along with the EOM, which acts like a capacitor, and the capacitor in parallel with it, create a resonant peak, as shown in blue in Figure 2.

The two inductor-capacitor pairs in parallel with these components create minima at two different frequencies, as shown in red in Figure 2. This occurs because, as the frequency approaches resonance, the impedance of the inductor-capacitor pair drops to zero, causing the voltage across the pair to drop to zero as well. Although the voltage across each component is large, the two voltages combine to exactly cancel out. When the effect of these components are combined, the response of the circuit results. The overall response of the circuit is shown in black in Figure 2. The frequency placement of the resonant peaks is manipulated by

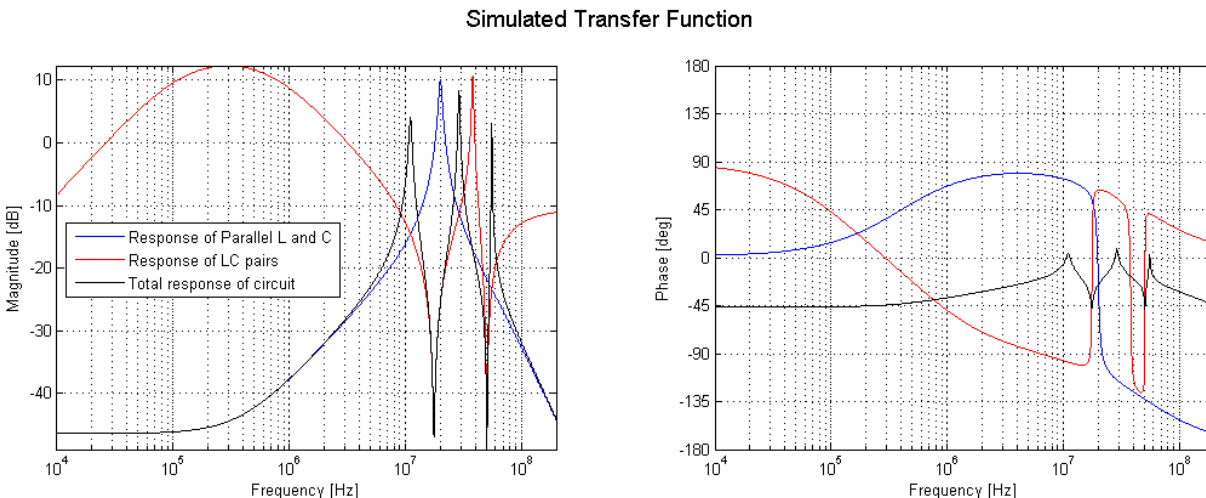


Figure 2: Theoretical performance of conceptual circuit

changing the inductor and capacitor values and thereby changing the placement of the main peak and two valleys. Resistors can be added to achieve the desired input impedance.

## 2.2 Specifications

For functioning in the advanced-LIGO length-sensing scheme, the EOM circuit must meet a few specifications. For the 40-m upgrade, the circuit must have resonant frequencies of 11 MHz, 29.5 MHz, and 55 MHz, so that the EOM will modulate the phase of the laser at those frequencies. The 29.5 MHz frequency will be used to control the mode cleaner, while the other two will be used for length sensing in the main interferometer. The EOM used will be a New Focus EOM KTP 4064, which has a phase-modulation depth of 13 mrad/V; since the optical modulation depth needs to be around 0.1 rad, the voltage across the EOM will need to be around 8.5 V at the 11 MHz and 55 MHz resonances. Since the available oscillators have a power of 13 dBm, the circuit will need to provide a minimum of 49.6 dB of gain. In addition to this, the impedance at each resonant frequency will need to be 50  $\Omega$  to avoid signal reflection back into the oscillator. The voltage across the EOM should also be roughly equivalent at 11 MHz and 55 MHz [4].

## 3 Circuit Testing

### 3.1 Initial Surface-Mount Circuit

Initially, a circuit was built using surface mount components on a board. A picture of this circuit is shown in Figure 3.

The transfer function of the circuit was then measured using an Agilent 4395A Network Analyzer. While the transfer function of this initial circuit did not look like the expected transfer function, the discrepancy could be explained to some extent by a short as shown in

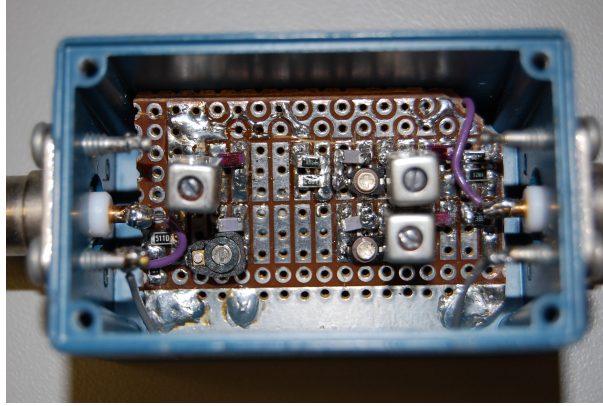


Figure 3: Picture of surface-mount circuit

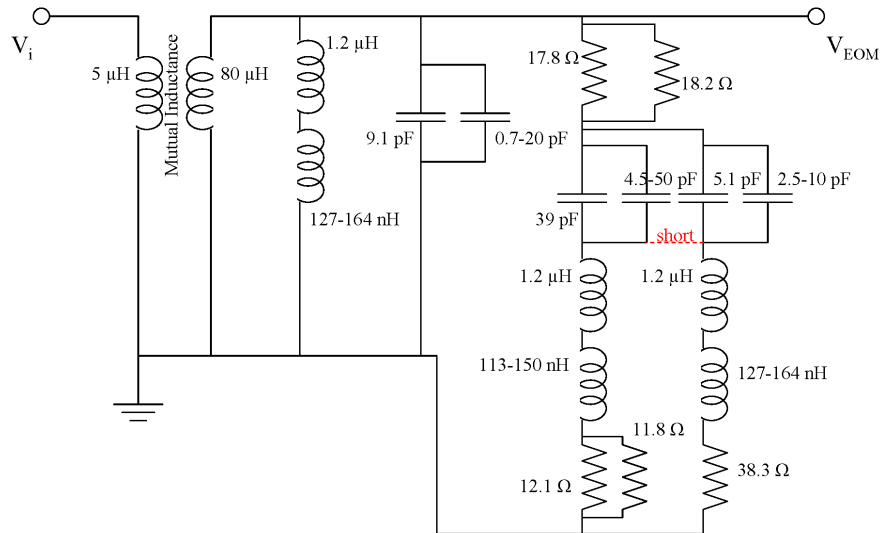


Figure 4: Circuit diagram of surface-mount circuit showing possible short in red

the circuit diagram in Figure 4. The transfer functions that were measured, simulated as designed, and simulated with a short are shown in Figure 5.

Even if the short is considered, the circuit did not perform as expected; this was likely due to imperfections in the construction of the circuit. One problem was with the construction of the board; for RF circuits, it is necessary to use a special type of board that orients the electrostatic fields in a specific direction.

### 3.2 Flying-Component Circuit

While flying-component circuits are not ideal for RF applications, it was decided that, since the relevant frequencies are below 100 MHz, a flying-component circuit could be used. This reduces the problems that can occur when using a board and the surface mount components.

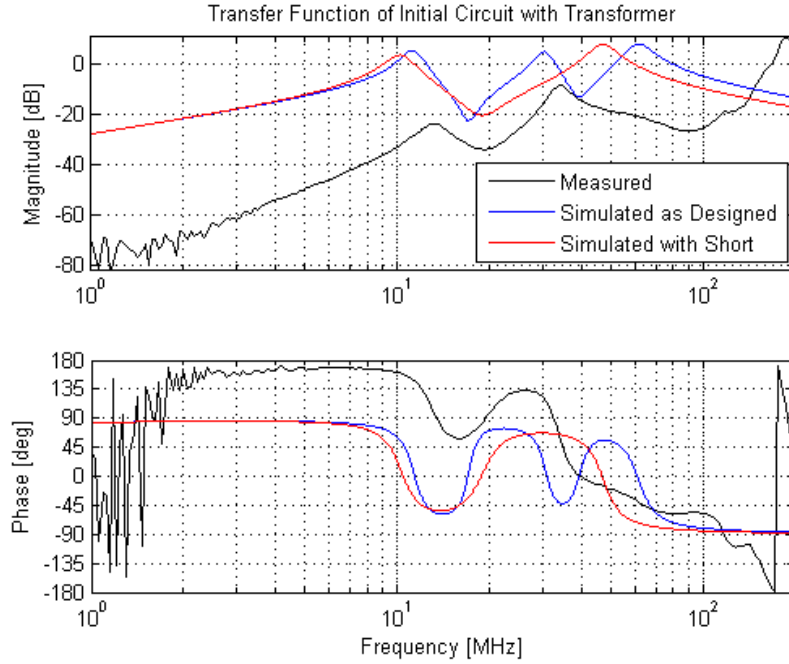


Figure 5: Measured and simulated transfer functions of the surface-mount circuit. Measured is shown in black, simulated in blue, and simulated with short in red.

A flying-component version of the circuit was built according to the circuit diagram in Figure 6. A picture of the circuit is shown in Figure 7.

Next, the transfer function of the circuit was measured; the measured and simulated transfer functions are shown in Figure 8. As can be observed from the figure above, the measured and simulated transfer functions were close to identical.

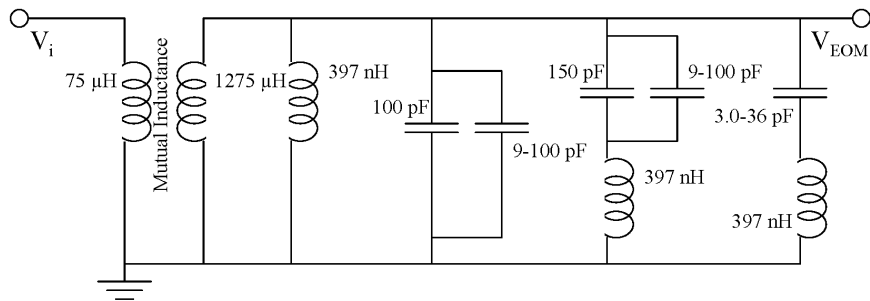


Figure 6: Circuit diagram of flying-component circuit

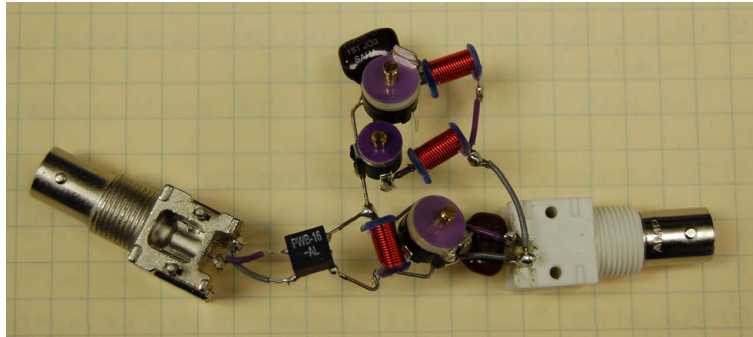


Figure 7: Picture of initial flying-component circuit

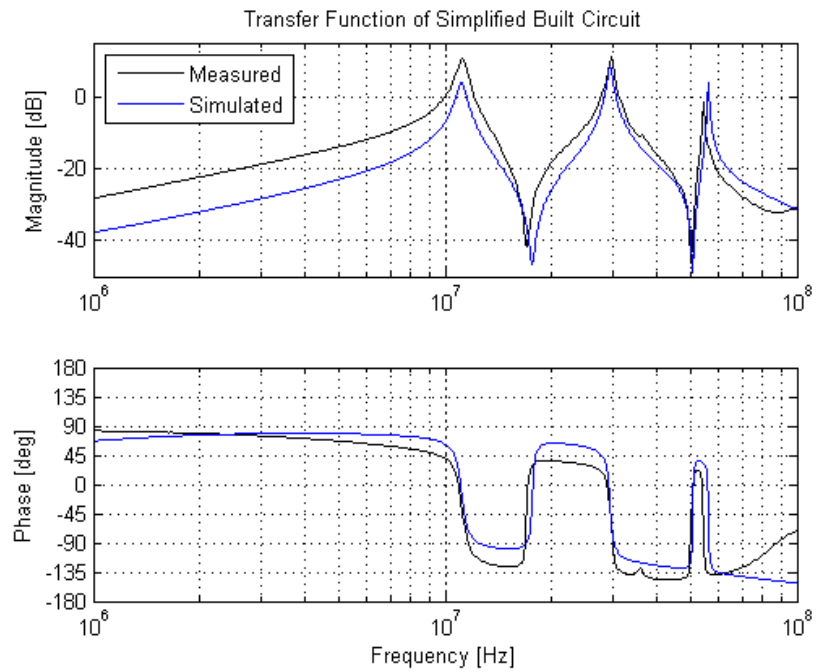


Figure 8: Measured and simulated transfer functions of flying-component circuit

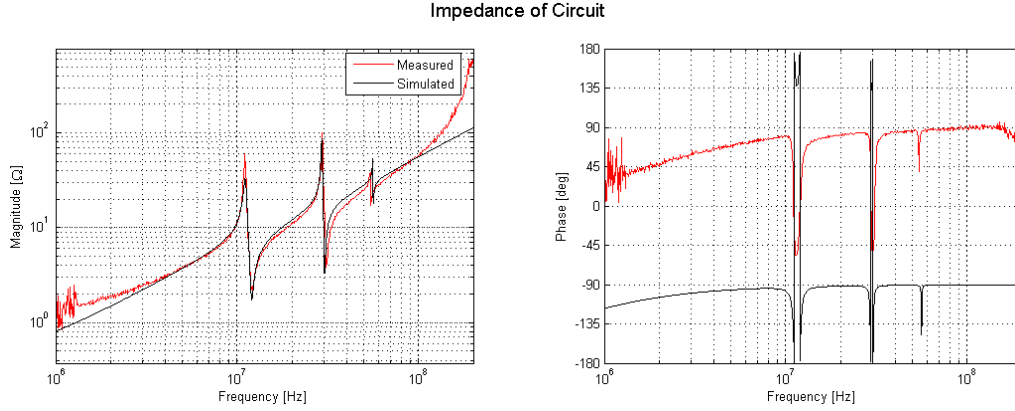


Figure 9: Initial impedance measurement shown with the expected impedance

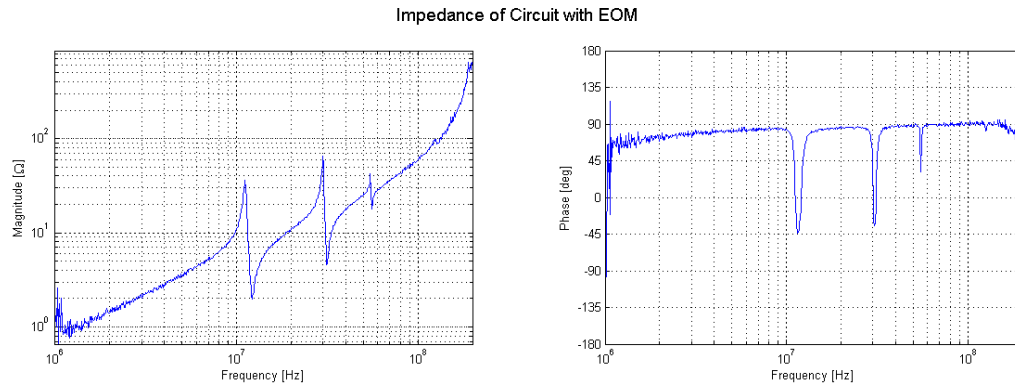


Figure 10: Impedance measurement of circuit attached to EOM

### 3.3 Impedance

Once it was determined that the transfer function of the circuit was functioning properly, it was necessary to measure the input impedance of the circuit to ensure that it was close to  $50 \Omega$  at the resonant peaks to prevent power reflection when the circuit is driven at those frequencies. The original impedance measurement is shown in Figure 9.

After the original measurement was taken, a capacitor was added to simulate the behavior of the circuit while attached to the EOM. The impedance was then adjusted using resistors until the impedance was at least the same order of magnitude as  $50 \Omega$ . Once this was done, the capacitor was removed, and the circuit was attached to the EOM; the impedance of this new setup was then measured. The final impedance of this circuit is shown in Figure 10. A circuit diagram showing the flying-component circuit attached to the EOM is shown in Figure 11. A picture of the circuit is shown in Figure 12.

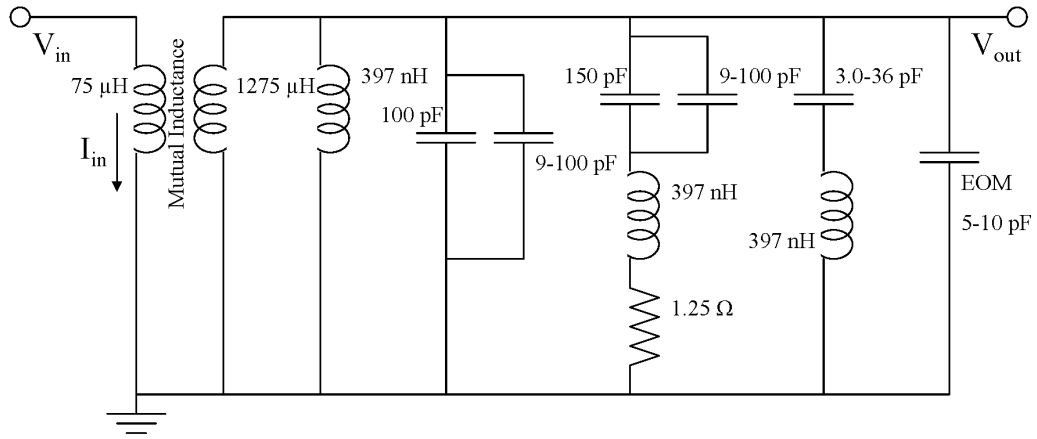


Figure 11: Circuit diagram for final flying-component circuit



Figure 12: Picture of flying-component circuit in box attached to EOM

### 3.4 Further Testing

Next, the circuit will be tested using an optical spectrum analyzer. The optical spectrum analyzer contains a scanning Fabry-Perot cavity; when the resonant frequency of the cavity is equal to the frequency of the laser, light is transmitted through the cavity to a photodetector. One of the mirrors is displaced using a piezoelectric mirror spacer driven by an oscillating voltage signal, thereby varying the resonant frequency of the cavity, and the frequency of light transmitted to the photodetector. Through this process, the intensity of light at each frequency can be determined and the spectral makeup of the beam can be analyzed. A diagram illustrating the setup for this test is shown in Figure 13. In addition to the optical spectrum analyzer, a broadband RF detector will also be used to observe and minimize unwanted amplitude modulation.

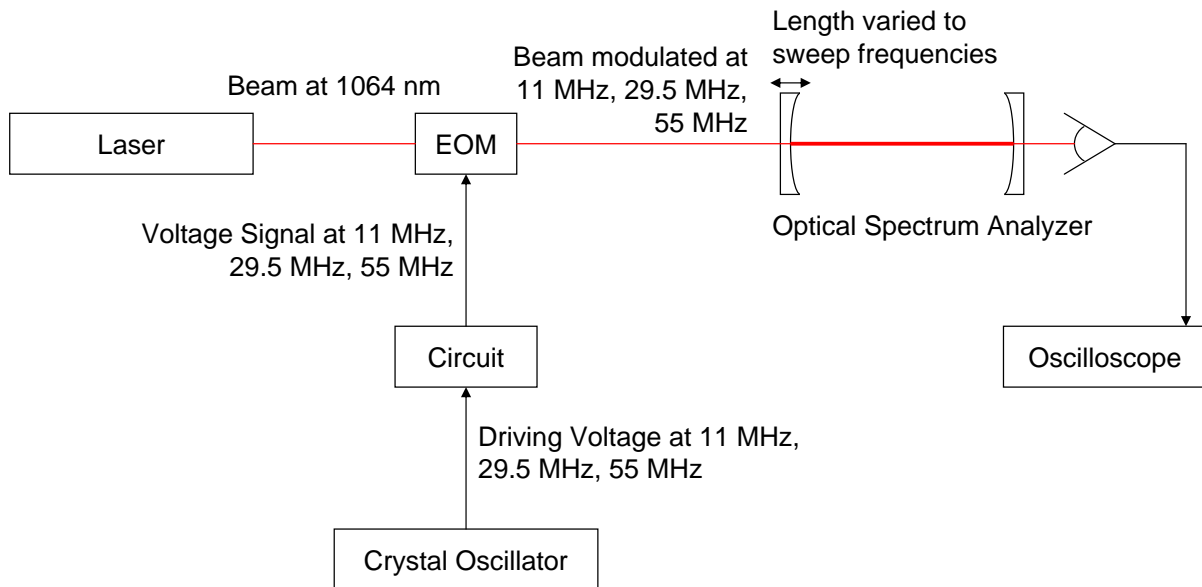


Figure 13: Optical spectrum analyzer setup

## 4 Future Work

The next step is to observe the modulations produced by the EOM using an optical spectrum analyzer. After that, any necessary modifications to the design will be made, and an improved prototype circuit may be built.

## 5 Summary and Conclusion

### A Methods

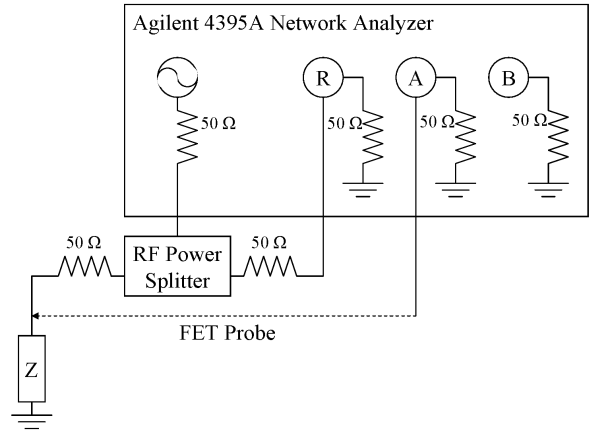


Figure 14: Schematic of impedance testing setup

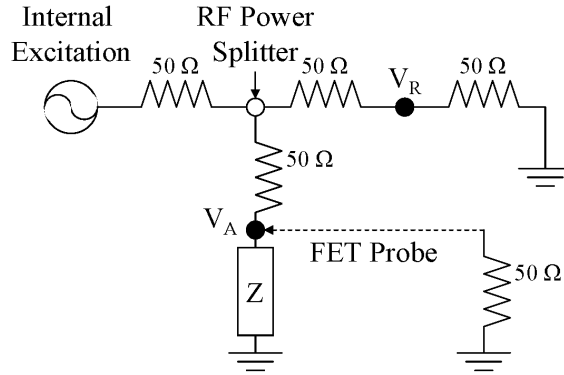


Figure 15: Circuit diagram showing the behavior of the impedance testing setup

### A.1 Impedance Measurement

An impedance measurement was made using the Agilent 4395A Network Analyzer. This was done by attaching both the A and R ports to the input terminals of the circuit and measuring the transfer function between them. If the network analyzer were ideal, this measurement would simply yield a transfer function of 1 (0 dB) for all frequencies; however, the electrical setup of the analyzer looks more like the diagram shown in Figure 14. For analysis purposes; the power splitter can be treated as a simple node, and the setup simplifies to the following circuit diagram (Figure 15). From this figure, it is possible to calculate that the transfer function is described by the following equation:

$$\frac{V_A}{V_R} = \frac{2Z}{Z + 50} \quad (1)$$

where  $Z$  is the impedance of the component being tested. In practice, attenuators must be used to prevent signal reflection back into the power splitter. A diagram of the actual setup is shown in Figure 16.

The system was then calibrated using a 50-Ω BNC termination, since the transfer function

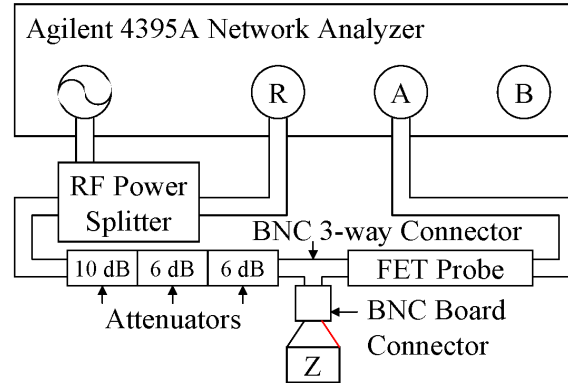


Figure 16: Schematic showing actual setup of Agilent 4395A for impedance testing

for that impedance should be 1 (0 dB) at all frequencies. Once the system was calibrated, and several impedances were tested to demonstrate that the system was functioning roughly as expected, the impedance of the circuit was measured.

## B Resources

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